

IMPROVED GAS FLOW FOR PLASMA ARC TORCH

FIELD OF THE INVENTION

The present invention relates to plasma arc torches and, more particularly, to a method and apparatus for supplying a gas flow for supporting an electric arc in a plasma arc torch.

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BACKGROUND OF THE INVENTION

Plasma arc torches are commonly used for the working of metal, including cutting, welding, surface treatment, melting, and annealing. Such torches include an electrode which supports an arc which extends from the electrode to a workpiece in the transferred arc mode of operation. It is also conventional to surround the arc with 10 a swirling vortex flow of gas, and in some torch designs it is conventional to also envelop the gas and arc in a swirling jet of water.

The electrode used in conventional torches of the described type typically comprises an elongate tubular member composed of a material of high thermal conductivity, such as copper or a copper alloy. The forward or discharge end of the 15 tubular electrode includes a bottom end wall having an emissive element embedded therein, which supports the arc. The emissive element is composed of a material which has a relatively low work function, which is defined in the art as the potential step, measured in electron volts (ev), which permits thermionic emission from the surface of a metal at a given temperature. In view of this low work function, the 20 element is thus capable of readily emitting electrons when an electrical potential is applied thereto. Commonly used emissive materials include hafnium, zirconium, tungsten, and alloys thereof. A nozzle surrounds the discharge end of the electrode and provides a pathway for directing the arc towards the workpiece.

A problem associated with torches of the type described above is the short service life of the electrode, particularly when the torch is used with an oxidizing gas, such as oxygen or air. More particularly, the emissive elements of these torches often erode below the surface of the copper holder at the discharge end. Additionally, the 5 gas tends to rapidly oxidize the copper of the electrode that surrounds the emissive element and, as the copper oxidizes, its work function decreases. As a result, a point is reached at which the oxidized copper surrounding the emissive element begins to support the arc, rather than the emissive element. When this happens, the copper oxide and the supporting copper melt, resulting in early destruction and failure of the 10 electrode.

In order to prevent or reduce the formation of oxidized copper surrounding the emissive element, particularly for air cooled plasma arc torches, the air is circulated rapidly about the electrode to improve heat transfer from the arc away from the electrode. A conventional method for the air to be distributed in an air cooled plasma 15 arc torch is for the air to first be used in some fashion to cool the electrode and then to be split into separate primary and secondary flows. Typically, this is accomplished by means of a gas baffle positioned between the nozzle and the electrode for splitting the flow into the primary or cutting gas flow and the secondary or shield gas flow, which helps maintain the position of the arc. More specifically, the primary flow of the gas 20 passes through holes in the gas baffle into a chamber defined by a primary nozzle and the electrode and is ejected by the primary nozzle, while the rest of the gas is directed out a secondary nozzle so as to surround the primary gas flow. Disadvantageously, the baffle splits the gas into the primary flow and secondary flow before the nozzle chamber, which limits the ability of the torch to transfer heat from the electrode and 25 can reduce the speed of the torch, as discussed below.

Baffles also add to the cost and complexity of manufacturing and assembling the torch. More specifically, baffles are subject to failure and can occasionally be inadvertently omitted by an operator during assembly of the torch. Furthermore, baffles tend to become brittle over time and eventually develop cracks, which often 30 lead to catastrophic failure unless the baffles are frequently replaced. Even when

replaced on a regular preventative maintenance cycle, which adds further cost to the torch, human error may lead to the baffles being left out during assembly of the torch, which can damage the torch or cause the torch to operate incorrectly. In addition, baffles can also permit the arc to "jump" or track across the baffle, which can also 5 damage the torch. Specifically, the use of baffles can result in a convoluted set of passages in and around the electrode through which air can pass, which can lead to migration of the arc through the passages. Although attempts have been made to insulate the labyrinth of passages through the torch, arcing through the often damp air in the passages has been a problem with conventional torches.

10 Another problem with conventional torches is the lack of cooling achieved by the gas due to splitting the gas into different flows before the gas has circulated along substantially the entire length of the electrode. In particular, many torches split the gas into the primary and secondary flows at a location intermediate the opposite ends of the electrode. This is considered necessary in order to limit the pressure realized in 15 the nozzle chamber while providing adequate flow for cooling. In order to cool the torch while avoiding failure of the torch due to excessive nozzle pressure, often as much as 70-90% of the total gas supplied to a conventional torch is diverted away from the nozzle chamber to other outlets, which direct the secondary flow. As a result, only a portion of the total gas supplied to the torch is available for cooling the 20 electrode along substantially the entire length of the electrode, and even less gas pressure than is optimal may be available at the exit end of the nozzle as a primary gas flow. Accordingly, conventional torches have limited cutting speeds, which adds time and expense to the torch operation. It is desirable to provide a greater nozzle chamber pressure so that higher cutting speeds can be realized. This is a difficult proposition, 25 however, due to the limitations of conventional torches as described, and for the fact that most manufacturing locations and welding shops use standard "shop" air pressure that cannot be increased in order to increase the gas pressure in the nozzle chamber.

30 Several patents discuss plasma arc torches having various flow patterns. For example, U.S. Patent No. 5,726,415 to Luo et al. discloses a plasma arc torch with an electrode having an metallic holder with an emissive element positioned at a discharge

end thereof. The torch also includes a nozzle, which in combination with the holder defines an annular gas chamber therebetween for directing a cooling gas about the electrode. The nozzle also defines a cylindrical exhaust port for directing a primary gas flow towards a workpiece, and bleed ports positioned in the rear portion of the
5 nozzle for venting a majority of the gas through bores for use as a shield or secondary gas flow. In operation, the bleed ports bleed approximately 90% of the gas, thus leaving 10% of the gas to cool the full length of the electrode and exit the cylindrical exhaust port as the primary gas flow towards the workpiece. Thus, only a fraction of the gas entering the torch travels substantially the length of the electrode, which
10 decreases the cooling capability of the gas.

U.S. Patent No. 4,558,201 to Hatch discloses a plasma arc torch having a reversible electrode that has both a forward insert and a rearward insert positioned at opposing ends thereof. The electrode defines a plurality of passageways for directing the gas towards a workpiece. In particular, gas is directed through channels around
15 the exterior of the electrode as well as through a central passage extending along the longitudinal axis of the electrode. As the gas reaches the midpoint of the electrode, however, the gas is split into a primary flow and a secondary flow, wherein the secondary flow is directed away from the electrode around an insulator to a front portion of a chamber defined by a nozzle and the insulator. The primary flow is
20 directed out a central orifice in the nozzle along with the electrical arc extending from the forward emissive insert to the workpiece. As in the Luo '415 patent, the gas flow is split into a primary flow and a secondary flow before the gas has traveled substantially the length of the electrode, which decreases the heat transfer capability of the gas and provides less gas pressure in the nozzle chamber, which decreases the
25 efficiency of the torch.

Thus, there is a need to provide sufficient gas flow to the torch in order to transfer heat away from the arc and the torch, but without sacrificing cutting speed or pressure realized in the nozzle chamber. It is also desirable to provide a torch with simple assembly and without using baffles to direct a flow of gas from the electrode to
30 the nozzle chamber.

SUMMARY OF THE INVENTION

The above and other objects and advantages of the present invention are achieved by a plasma arc torch that directs a flow of gas along substantially the length of the electrode such that more gas is used to cool the torch compared to conventional 5 torches. The torch of the present invention includes an electrode defining a plurality of openings positioned proximate the front end of the electrode such that all of the gas supplied to the torch is directed through the openings into a chamber defined by the electrode and the nozzle. In this regard, the gas pressure in the nozzle chamber is increased compared to conventional torches, which allows the torch of the present 10 invention to have a faster cutting speed. Advantageously, the torch of the present invention utilizes the openings in the electrode itself to direct the flow of gas, and not baffles as in conventional torches.

In particular, a plasma arc torch according to one embodiment of the present invention includes an electrode having an upper tubular member defining an internal 15 bore and a lower cup-shaped member or holder defining a central passageway in fluid communication with the internal bore of the upper tubular member. The front end of the holder defines a cavity for receiving an emissive insert, and the rear end defines the central passageway. The holder also defines a plurality of side openings that are in fluid communication with the central passageway. In one embodiment, the side 20 openings are arranged to impart a swirling motion to the gas flowing therethrough.

The plasma arc torch also includes a nozzle positioned proximate the front end of the holder such that a nozzle chamber is defined therebetween. The nozzle defines a central bore for discharging a primary flow of gas towards a workpiece, and in one embodiment also defines a plurality of secondary openings for creating a secondary 25 flow of gas therethrough. Advantageously, the openings defined in the nozzle and holder eliminate the need for separate baffles for separating the gas flow into the primary and secondary flows.

Safety items are also a part of the torch of the present invention. More specifically, in one embodiment a ball valve assembly is located in the internal bore of 30 the upper tubular member of the electrode for regulating gas flow through the

electrode. In this regard, the ball valve assembly acts to protect the torch from damage if a user attempts to operate the torch with portions of the torch missing, such as the holder of the electrode, by cutting off the gas flow through the torch. The plasma arc torch of the present invention can also include a pressure switch in fluid communication with the nozzle chamber. The pressure switch can disable the torch if the gas pressure in the torch, such as in the nozzle chamber, is below a predetermined value, which may occur if the torch is assembled incorrectly or if the torch is damaged.

Methods are also a part of the present invention. According to one method of the present invention, a electrode having a metallic holder is provided, wherein the holder defines a plurality of side openings and a central passageway in fluid communication therewith. A nozzle is positioned proximate the holder to define a nozzle chamber therebetween. A flow of gas is directed through the central passageway into the nozzle chamber such that all of the gas supplied into the central passageway is directed through the side openings into the nozzle chamber. Advantageously, the gas is split into at least a primary flow and a secondary flow after the flow of gas has entered the nozzle chamber, which provides greater pressure in the nozzle chamber and allows for greater cutting speeds. To improve the ability of the torch to transfer heat from the arc, the flow of gas is directed through the central passageway a distance more than 1/2 the length of the holder before being directed through the side openings thereof. As such, more gas is available for transferring heat from the arc and electrode away from the torch.

As mentioned above, the flow of gas can also be directed to certain safety devices, such as the flow-regulating ball valve assembly, or to the pressure switch that is in fluid communication with the nozzle chamber. Advantageously, the torch is disabled if certain conditions occur, such as having a gas pressure in the torch that is below a predetermined value.

Accordingly, the present invention provides a plasma arc torch that overcomes the disadvantages of conventional torches without sacrificing the cutting speed of the torch or the pressure realized in the nozzle chamber. Advantageously, the torch and

methods of the present invention avoid the use of baffles to direct the flow of gas from the electrode to a primary flow and a secondary flow, which improves the assembly, reliability, and cost of the torch.

BRIEF DESCRIPTION OF THE DRAWINGS

Having thus described the invention in general terms, reference will now be made to the accompanying drawings, which are not necessarily drawn to scale, wherein:

Figure 1 is a cross-sectional view of a front portion of a plasma arc torch according to the present invention;

10 Figure 2 is a detailed cross-sectional view of a portion of an electrode and a nozzle according to one embodiment of the present invention; and

Figure 3 is a detailed cross-sectional view taken along lines 3-3 of Figure 2 according to one embodiment of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

15 The present invention now will be described more fully hereinafter with reference to the accompanying drawings, in which preferred embodiments of the invention are shown. This invention may, however, be embodied in many different forms and should not be construed as limited to the embodiments set forth herein; rather, these embodiments are provided so that this disclosure will be thorough and 20 complete, and will fully convey the scope of the invention to those skilled in the art. Like numbers refer to like elements throughout.

Referring to the accompanying drawings, Figure 1 illustrates a preferred embodiment of a plasma arc torch, indicated generally at 10, according to the invention. The torch 10 comprises a torch body 20 and electrode 40 mounted within the torch body, and a handle 13 secured to the torch body, such as by press fitting over a plurality of bushings 14. The torch 10 further comprises a supply line 70 for directing a pressurized flow of gas through the torch body 20 and directing electrical power to the electrode 40. In one embodiment, the torch 10 also includes a detecting

device **80** for sensing the gas pressure in the torch body **20** and for disabling the flow of electrical current to the electrode **40** in accordance with the present invention.

As shown in Figure 1, the torch body **20** comprises a generally cylindrical head portion **21** defining a discharge axis. The head portion **21** includes a housing **22** surrounding a portion of the electrode **40** along the discharge axis. The housing **22** is typically made of a hard, heat-resistant material, such as thermoset plastic or epoxy compound, which protects the components of the torch from the high heat generated during plasma arc cutting. The electrode **40** includes an upper tubular member **23** and a lower cup-shaped member or holder **41**. The upper tubular member **23** defines an internal bore **24** which is coaxially aligned with the discharge axis. In one embodiment, the internal bore **24** includes a valve seat **34**, as discussed more fully below. The upper tubular member **23** is made of an electrically conductive material, preferably copper or copper alloy, such that the upper tubular member conducts an electrical current to other portions of the electrode **40**. The upper tubular member **23** also defines a passageway **25** such that the internal bore **24** is in fluid communication with the supply line **70**. In addition, a cap **26** is secured to the top of the upper tubular member **23** for directing gas along the discharge axis. In one embodiment, the upper tubular member **23** includes an internally threaded portion **27**.

The supply line **70** comprises a hollow conduit **72** defining a gas passageway and is positioned within the torch body **20**. The conduit **72** originates at a source of pressurized gas and terminates in the passageway **25** of the upper tubular member **23** of the electrode **40** such that the source of pressurized gas is in fluid communication with the internal bore **24**. Supply line **70** further comprises a power supply cable **71** electrically connected to the conduit **72** and a power source such that the power source is electrically connected to the electrode **40**.

Figure 2 illustrates one embodiment of the holder **41** of the electrode **40**. In particular, the holder **41** is made of an electrically conductive material, preferably copper or copper alloy. The holder **41** has a rear end **42** defining a central passageway **43** that is in fluid communication with the internal bore **24** of the upper tubular member **23**. In one embodiment, the rear end **42** includes a plurality of external

threads 44 suitable for threadably engaging the internally threaded portion 27 of the upper tubular member 23. The holder 41 also includes a front end 45 having a front face 46 and defining a front cavity or opening 47 therein. The holder 41 includes side walls 48 and a transverse end wall 49 that define the central passageway 43.

5 The holder 41 also defines a plurality of openings 50 that are positioned in the side walls 48 adjacent the end wall 49. Advantageously, the openings 50 are located at a position less than one-half the length of the holder 41 from the front face 46 thereof. In a preferred embodiment, the openings 50 are located proximate the end wall 49 of the holder 41 at the forward end of the central passageway 43 and, 10 according to one embodiment, are directed non-radially so that gas passing through the openings is swirled about the holder 41. In one embodiment shown in Figure 3, the end wall 49 defines a plurality of channels 56 corresponding to the openings 50 for directing the gas from the central passageway 43 through the openings. As discussed below, gas is directed through the supply line 70 and into the internal bore 24 of the 15 upper tubular member 23. The gas is then directed into the central passageway 43 of the holder 41 towards the openings 50 so as to cool the electrode while the torch 10 is in use. To further the cooling action of the gas, a channeled valve pin 51 can be positioned in the internal bore 24 and central passageway 43 for increasing the 20 velocity of the gas therein, such as by swirling the gas. In this manner, the gas receives more contact with the electrode 40, which thereby increases the heat transfer between the electrode and the gas. The pin 51 can also be used as a safety device, as discussed more fully below.

25 In one embodiment, the front end 45 of the holder 41 includes an emissive element 52 disposed in the opening 47. The emissive element 52 acts as the cathode terminal for an electrical arc extending from the front end of the electrode 40 in the direction of a workpiece WP, as discussed more fully below. For example, an electrode comprising an emissive element is disclosed in U.S. Patent No. 5,023,425 to Severance, Jr., and assigned to the assignee of the present invention. The emissive element 52 is composed of a material which has a relatively low work function, 30 defined in the art as the potential step, measured in electron volts, that permits

thermionic emission from the surface of a metal at a given temperature. In view of its low work function, the emissive element readily emits electrons in the presence of an electrical potential. Commonly used insert materials include hafnium, zirconium, tungsten, and alloys thereof.

5 In addition, a relatively non-emissive separator (not shown) may also be positioned about the emissive element **52** at the front end **45** of the holder **41**. In particular, the separator is positioned about the emissive element **52** in the opening **47** of the electrode. The separator is composed of a metallic material having a work function which is greater than that of the material of the holder **41**, and also greater
10 than that of the material of the emissive element **52**. In this regard, it is preferred that the separator be composed of a metallic material having a relatively high work function. Several metals and alloys are usable for the non-emissive separator of the present invention, such as silver, gold, platinum, rhodium, iridium, palladium, nickel.
15 The emissive element **52**, separator, and holder **41** are flush with one another at the front face **46** of the holder.

As shown in Figure 2, the torch **10** also includes a nozzle **60** positioned proximate the holder **41** of the electrode **40**. The nozzle **60** includes an upper portion **61**, a middle portion **62**, and a frustoconical lower portion **63**. The nozzle **60** is positioned about the holder **41** such that a chamber **90** is defined therebetween. The upper portion **61** of the nozzle **60** defines a plurality of slots **65** through which air pressure from the nozzle chamber **90** is communicated to the detecting device **80**.
20 The middle portion **62** of the nozzle forms a shoulder **64** with the upper portion **61** and defines a plurality of openings **66** therethrough such that the nozzle chamber **90** is in fluid communication with a shield or secondary gas flow port **91**, which is defined
25 between the nozzle **60** and an outer heat shield **74** and is in fluid communication with the ambient atmosphere (see Figure 1). The lower portion **63** of the nozzle **60** defines a central bore **67** for discharging gas from the nozzle chamber **90** toward the workpiece **WP** located adjacent the nozzle.

The nozzle **60** is held in place about the holder **41** by the outer heat shield **74**.
30 In one embodiment, the heat shield **74**, which is preferably formed of an electrically

insulating material, includes a metallic sleeve 92 having a transverse portion 93 at one end and threaded portion 76 at the other end. The threaded portion 76 threadably engages a threaded surface 79 of the housing 22, and the transverse portion 93 engages the shoulder 64 provided on the nozzle 60 to hold the nozzle in place about 5 the holder 41 when the heat shield 74 is secured on the torch body 20. Once installed, the heat shield 74 also defines a central opening 78 therethrough adjacent the nozzle 60 and coaxially aligned with the discharge axis such that the shield gas port flow 91 is defined between the heat shield and nozzle. A resilient O-ring 77 is positioned between the housing 22 and the heat shield 74 to protect the electrode 40 and nozzle 10 60 from external contaminants and to seal the torch body 20 when the heat shield is properly secured thereto.

The pressure detecting device 80 comprises a hollow conduit 82 defining a gas passageway within the torch body 20. More specifically, conduit 82 originates in the head portion 21 of torch body 20, and terminates at a pressure switch (not shown) 15 such that the pressure switch is in fluid communication with the internal bore 24 of the upper tubular member 23 and the central passageway 43 of the holder 41 via the side openings 50 and the slots 65. The conduit 82 and pressure switch of this type are described in U.S. Patent No. 5,681,489, which is assigned to the assignee of the present invention and incorporated herein by reference.

20 In operation, when an operator presses a control switch (not shown), a low voltage electrical circuit in the power source is closed. The electrical circuit opens a solenoid positioned in the power source such that the supply line 70 directs a singular, pressurized flow of gas through the conduit 72 to the head portion 21 and internal bore 24 of the upper tubular member 23. The pressurized gas may be any gas capable 25 of forming a plasma flow, but preferably is air, oxygen or nitrogen. The gas is then directed to the central passageway 43 defined in the holder 41. Advantageously, all of the gas supplied into the central passageway 43 exits through the openings 50 positioned adjacent the end wall 49 of the holder 41 and into the nozzle chamber 90. Thus, the gas travels substantially the length of the electrode 40, such as to a position 30 less than one-half the length of the electrode 40, and preferably one-half the length of

the holder 41, measured along the longitudinal axis from the front face 46. As such, the torch of the present invention provides improved cooling to the electrode compared to conventional torches. As noted above, the openings 50 are preferably in a tangential formation, as shown in Figure 3. This arrangement creates a swirling 5 pattern about the front end 45 as the gas enters the nozzle chamber 90.

After the gas arrives in the nozzle chamber 90 via the openings 50, a primary flow portion of the gas is directed to the central bore 67 of the nozzle 60. In addition, the opening 66 defined in the middle portion 62 of the nozzle 60 allow a secondary flow portion of the gas to escape therethrough to the shield gas flow port 91. Thus, all 10 of the gas present in the nozzle chamber 90 enters the nozzle chamber through the openings 50 in the holder 41. In this manner, higher nozzle pressures can be achieved, which allows for a higher cutting speed of the torch 10. Moreover, the gas is in contact with the electrode 40 for a longer period of time compared to conventional torches, which improves cooling of the torch.

15 As mentioned above, the flow of gas is initiated by an operator pressing a control switch. In order to supply electricity to the electrode, sufficient gas pressure must be present in the torch. More specifically, when the outer heat shield 74 is properly secured about the nozzle 60 on the torch body 20, the pressure detecting device 80 senses the gas pressure in the torch body, such as in the nozzle chamber 90. 20 According to one embodiment of the present invention, the pressure in the nozzle chamber 90 should be at least approximately 30 psi using conventional "shop" air, which is about 75 psi. If the device 80 senses sufficient gas pressure in the nozzle chamber 90 for a predetermined time, typically about three seconds, the detecting device closes, or causes to be closed, an electrical circuit to permit the power source to 25 supply electrical current to the torch 10. In other words, as long as there is sufficient gas pressure in the nozzle chamber 90, which can be achieved by maintaining a predetermined gas flow rate through a properly assembled torch, the power source will supply electrical current to the electrode 40.

30 If, however, there is insufficient gas pressure in the torch body 20, such as when the nozzle 60 is removed or misaligned, or if the heat shield 74 is removed, the

pressurized gas flows through the openings **50** and primarily out the front of the torch to the atmosphere, so that substantially no gas enters the conduit **82** of the pressure detecting device **80**. As a result, sufficient pressure of the gas is not sensed at the pressure switch via the conduit **82**, which ceases electrical current to the electrode **40**.

5 In one embodiment, the torch **10** also includes a ball valve assembly capable of regulating the gas through the torch. In particular, the assembly includes a non-conductive ball **33** of spherical geometry that is positioned in the internal bore **24** of the upper tubular member **23** and is biased by a bias member **35**, such as a spring, against the valve seat **34**.

10 The valve pin **51** is capable of moving and holding the ball **33** away from the valve seat **34** when the holder **41** is properly installed and engaged with the upper tubular member **23**. In particular, the ball **33** serves as a "parts in place" feature to protect the torch body **20** from damage should the holder **41** or valve pin **51** be left out. If either is omitted, the ball **33** remains against the valve seat **34**, which prevents 15 the gas from flowing through the internal bore **24** to the central passageway **43**. As a result, the lack of gas flow prevents a pressure signal from being communicated to the pressure switch via the conduit **82**, which must be satisfied for the power source to deliver current to the torch **10**. Such a feature is described in U.S. Patent No. 4,580,032 to Carkhuff, which is assigned to the assignee of the present invention and 20 incorporated herein by reference.

Thus, the present invention provides a plasma arc torch and method of directing a flow of gas in the torch such that greater cooling of the electrode is achieved and increased cutting speeds can be realized compared to conventional torches. In particular, the electrode of the present invention provides a holder defining 25 a plurality of openings proximate the front end thereof for directing all of the gas into the nozzle chamber before splitting the gas into primary and secondary flows. As such, the gas is in contact with the electrode along substantially the length of the electrode before it is split, which improves cooling of the electrode. Furthermore, gas baffles are not used in assembly of the torch to separate the gas into primary and 30 secondary flows. In this regard, the assembly time and cost of the torch are reduced,

while providing an increase in nozzle chamber pressure and thus cutting speed of the torch.

Many modifications and other embodiments of the invention will come to mind to one skilled in the art to which this invention pertains having the benefit of the teachings presented in the foregoing descriptions and the associated drawings. For example, the sensing device and other safety features of the present invention are not mandatory in order to benefit from the teachings presented herein, but are recommended for operator safety and torch life. Therefore, it is to be understood that the invention is not to be limited to the specific embodiments disclosed and that modifications and other embodiments are intended to be included within the scope of the appended claims. Although specific terms are employed herein, they are used in a generic and descriptive sense only and not for purposes of limitation.